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University of Applied Sciences

Laboratory for Building Materials at the University of Applied Sciences, Augsburg

Subject:

Tests on cementitious screeds

Ordering party:

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1. Introduction

The Laboratory for Building Materials at the University of Applied Sciences, Augsburg, was ordered by Mr Alexander Unger (ordering party, below referred to as "op") to conduct experiments with mortars for floating screeds, based on a novel formulation.

The experiments are to determine the material behaviour of the tested screeds in relation to a comparison mixture (usual screed mixture used at building lots).

The experimental set-up, the test procedure and the manufacture of sample areas were discussed with the "op" and were realized according to valid international test standards.

The experiments were conducted by Mr Tobias Keller, graduate engineer, in the period between 29 June 2007 and 24 October 2007.

2. Test procedure

All in all, six screeds were installed within two settings (2 plus 4) as floating load-bearing layers. The details are shown in the following illustrations and tables:

| Series | Area no. | Mixture | Date of installation | Bottom section [mm] | Thickness [mm] | Nature | Dimension [m] |
|--------|-------------|-----------------------|----------------------|---------------------------|-------------------|----------|------------------|
| 1 | 1 | RenoScreed | 04.07.07 | 20 | 35 | Unheated | 2.70 x 3.60 |
| 1 | 2 | Comparison mixture | 04.07.07 | 20 | 35 | Unheated | 2.70 x 3.60 |
| 2 | 1 | RenoScreed | 13.08.07 | 20 | 35 | Heated | 1.35 x 1.80 |
| 2 | 2 | RenoScreed | 13.08.07 | 20 | 55 | Unheated | 1.35 x 1.80 |
| 2 | 3 | Comparison mixture | 13.08.07 | 20 | 45 | Heated | 1.35 x 1.80 |
| 2 | 4 | Comparison mixture | 13.08.07 | 20 | 65 | Unheated | 1.35 x 1.80 |

 Table 1: Overview of the sample areas.

The following illustrations give an overview of the position of the sample areas in the basement of the laboratory of building materials at the University of Applied Sciences Augsburg (Temperature: $11 - 18^{\circ}$ C; 65 - 90 % rel. humidity).



Illustration 1: Overview of the installed sample areas, 1st experimental series (=ES).



Illustration 2: Overview of the installed sample areas, 2nd ES.

The formulation of the compositions was specified by the "op" and was not communicated to the laboratory.

3. Test results

3.1 Curling behaviour

To measure the curling behaviour on each of the sample areas, an electronic displacement transducer was installed in each of the four corners and in the centre of the slab. The values measured by these five electronic displacement transducers were recorded throughout the test period. The two following illustrations show the edge curling behaviour of the two mixtures from the first experimental series:



Illustration 3: Edge curling; 1^{st} ES (comparison mixture); RH = Relative Humidity; (N) = comparison mixture.



Illustration 4: Edge curling; 1st ES (*RenoScreed*); RH = Relative Humidity; (R) = *RenoScreed*.

On 1 August 2007 the surface of both screeds was watered by means of a hose and the water was evenly spread with a brush. The resulting resilience values are shown in the illustrations below:



Illustration 5: Deformation of the comparison mixture after watering $(1^{st} ES)$; (N) = comparison mixture.



Illustration 6: Deformation of *RenoScreed* after watering $(1^{st} ES); (R) = RenoScreed$.



Illustration 7: Edge curling; 2^{nd} ES (comparison mixture); RH = Relative Humidity; (N65) = comparison mixture, 65 mm.



Illustration 8: Edge curling; 2nd ES (comparison mixture); RH = Relative Humidity; (N45) = comparison mixture, 45 mm.



Illustration 9: Edge curling; 2nd ES (*RenoScreed*); RH = Relative Humidity; (R55) = *RenoScreed*, 55 mm.

Two of the five electronic displacement transducers of that experimental slab broke down during the measurement, so they could not be used to determine the edge curling.



Illustration 10: Edge curling; 2nd ES (*RenoScreed*); RH = Relative Humidity; (R35) = *RenoScreed*, 35 mm.

The following graphs illustrate the resilience of the screeds which were watered on 5 October 2007.



Illustration 11: Resilience; 2nd ES (comparison mixture); (N65) = comparison mixture, 65 mm.



Illustration 12: Resilience; 2nd ES (comparison mixture); (N45) = comparison mixture, 45 mm.



Illustration 13: Resilience; 2nd ES (*RenoScreed*); (R55) = *RenoScreed*, 55 mm.



Illustration 14: Resilience; 2nd ES (*RenoScreed*); (R35) = *RenoScreed*, 35 mm.

In order to establish the behaviour of the comparison mixture and *RenoScreed* under stone and ceramic floorings on 29 November 2007 standard tiles were placed on all four sample areas.

Before laying the tiles the sample areas were cut into equal dimensions of 1.80 m x 1.30 m. As material for the tiles porcelain stoneware with an edge length of 34 x 34 cm and a thickness of 6 mm was used. It was glued to the screed with the help of 'PCI Nanolight' adhesive. The tiles were jointed right after the bonding to the screed with 'PCI Nanofug'.

The sample areas produced with the comparison mixture and with the *RenoScreed* mixture were examined on 15 February 2008. No damage could be established on both screed samples and on the tiles (e. g. in the form of cracks).

3.2 Drying process (moisture contents [% w/w])

- CM-moisture test
- Drying kiln test
- Electronic measurement

(1, 3, 7, 12, 13, 14 and 28 days after the screeds were laid)

[measuring devices: "Denzel" = G812 – "Gann" = Hydromette M4050 + B50]

| Derra | Kiln-dried | Kiln-dried (105°C) | | СМ | СМ | СМ | "Gann"- | "Denzel"- |
|--------------|------------|--------------------|-------|--------|--------|--------|---------|-----------|
| Days | (≈ 250°C) | Slab | Prism | 10 min | 30 min | 60 min | method | method |
| After laying | 9.8 | - | - | - | - | - | - | - |
| 1 d | 8.4 | 7.6 | 7.6 | - | 6.4 | 6.5 | - | - |
| 3 d | 6.8 | 6.5 | 6.8 | - | - | 4.4 | - | 6.5 |
| 7 d | - | 5.1 | 6.5 | - | 3.7 | 4.2 | > 5.9 | - |
| 12 d | - | 4.6 | - | 1.1 | 1.6 | - | > 5.9 | 4.8 |
| 13 d | - | - | - | 1.6 | 2.2 | - | - | - |
| 14 d | - | 4.7 | 3.2 | 1.9 | 2.4 | - | > 5.9 | 5.2 |
| 28 d | - | 3.9 | 1.8 | 1.9 | 2.4 | - | 5.8 | 4.7 |

Table 2: Moisture contents [% w/w]; 1st ES (comparison mixture).

| Dave | Kiln-dried (≈ 250°C) | Kiln-dried (105°C) | | СМ | СМ | СМ | "Gann"- | "Denzel"- |
|--------------|-------------------------|--------------------|-------|--------|--------|--------|---------|-----------|
| Days | | Slab | Prism | 10 min | 30 min | 60 min | method | method |
| After laying | 8.1 | - | - | - | - | - | - | - |
| 1 d | 6.4 | 5.6 | 5.9 | - | 4.8 | 4.9 | - | - |
| 3 d | 5.7 | 4.7 | 5.3 | - | 1.9 | 2.5 | - | 5.5 |
| 7 d | - | 4.3 | 5.2 | - | 2.9 | 3.2 | 5.7 | - |
| 12 d | - | 4.2 | - | 0.5 | 0.8 | - | 5.9 | 4.9 |
| 13 d | - | - | - | 0.7 | 1.2 | - | - | - |
| 14 d | - | 3.6 | 3.3 | 1.7 | 2.2 | - | 5.8 | 4.4 |
| 28 d | - | 3.0 | 2.5 | 1.7 | 2.3 | - | 5.8 | 4.7 |

Table 3: Moisture contents [% w/w]; 1st ES (*RenoScreed*).

The moisture content values of the second experimental series are presented in the subsequent tables:

| Derra | Kiln-dried | Kiln-dried (105°C) | | СМ | СМ | СМ | "Gann"- |
|--------------|------------|--------------------|-------|--------|--------|--------|---------|
| Days | (≈ 250°C) | Slab | prism | 10 min | 30 min | 60 min | method |
| After laying | 11.0 | | | | | | |
| 1 d | 9.6 | 9.0 | 8.2 | 8.9 | 9.5 | - | 10.0 |
| 3 d | 7.7 | 7.2 | 7.6 | 5.9 | 6.7 | - | 6.2 |
| 7 d | - | 6.4 | 7.6 | 4.4 | 5.2 | > 5.9 | 5.5 |
| 14 d | - | 5.6 | 7.2 | 3.3 | 4.1 | - | 5.4 |
| 28 d | - | 5.5 | 3.6 | 3.6 | 4.4 | 5.8 | 4.6 |
| 56 d | - | 4.8 | - | 1.9 | 2.4 | 3.5 | - |

Table 4: Moisture contents [% w/w] of the comparison mixture (65 + 20 mm), 2^{nd} ES.

| Dava | Kiln-dried | Kiln-dried (105°C) | | СМ | СМ | СМ | "Gann"- |
|--------------|------------|--------------------|-------|--------|--------|--------|---------|
| Days | (≈ 250°C) | Slab | prism | 10 min | 30 min | 60 min | method |
| After laying | 11.0 | | | | | | |
| 1 d | 10.0 | 7.5 | 8.2 | 9.5 | 10.0 | - | 10.0 |
| 3 d | 9.1 | 7.9 | 7.6 | 4.9 | 5.9 | - | 6.3 |
| 7 d | - | 7.5 | 7.6 | 4.4 | 5.8 | > 5.9 | 5.8 |
| 14 d | - | 6.4 | 7.2 | 2.8 | 3.4 | - | 4.8 |
| 28 d | - | 5.6 | 3.6 | 3.6 | 4.2 | 5.8 | 4.5 |
| 56 d | - | 4.7 | - | 2.7 | 2.9 | 4.0 | 3.4 |

Table 5: Moisture contents [% w/w] of the comparison mixture (45 + 20 mm), 2^{nd} ES.

| Davia | Kiln-dried | Kiln-dried (105°C) | | СМ | СМ | СМ | "Gann"- |
|--------------|------------|--------------------|-------|--------|--------|--------|---------|
| Days | (≈ 250°C) | Slab | prism | 10 min | 30 min | 60 min | method |
| After laying | 8.2 | - | - | - | - | - | - |
| 1 d | 6.8 | 6.0 | 6.0 | 4.6 | 5.0 | - | 5.5 |
| 3 d | 5.5 | 4.8 | 5.1 | 3.4 | 4.0 | - | 4.8 |
| 7 d | - | 4.7 | 5.2 | 1.4 | 1.9 | 2.8 | 4.3 |
| 14 d | - | 4.2 | 5.1 | 1.0 | 1.5 | 2.3 | 4.5 |
| 28 d | _ | 4.1 | 3.8 | 1.9 | 2.3 | 5.5 | 4.2 |
| 56 d | _ | 3.9 | - | 0.9 | 1.2 | 3.4 | 3.9 |

Table 6: Moisture contents [% w/w] of *RenoScreed* (55 + 20 mm), 2^{nd} ES.

| Dave | Kiln-dried | Kiln-dried (105°C) | | СМ | СМ | СМ | "Gann"- |
|--------------|------------|--------------------|-------|--------|--------|--------|---------|
| Days | (≈ 250°C) | slab | prism | 10 min | 30 min | 60 min | method |
| After laying | 8.2 | - | - | - | - | - | - |
| 1 d | 6.3 | 5.5 | 6.0 | 3.8 | 4.9 | - | 5.4 |
| 3 d | 5.7 | 4.5 | 5.1 | 4.5 | 6.0 | - | 5.0 |
| 7 d | - | 4.5 | 5.2 | 1.2 | 1.7 | 2.4 | 4.5 |
| 14 d | - | 4.0 | 5.1 | 1.2 | 1.7 | 5.1 | 4.8 |
| 28 d | - | 3.9 | 3.8 | 1.9 | 2.3 | 5.1 | 4.0 |
| 56 d | - | 3.7 | - | 1.0 | 1.6 | 3.7 | 4.3 |

Table 7: Moisture contents [% w/w] of *RenoScreed* (35 + 20 mm), 2nd ES.

3.3 Shrinkage behaviour (prisms [4 x 4 x 16 cm] storage under conditions equal to the sample areas)

While manufacturing the sample areas, 6×3 prisms were extracted from each mixture. Three prisms from each mixture were stored next to the sample areas, which were measured regularly to record the shrinkage deformation.



Illustration 15: Shrinkage of prisms; 1st ES.



Illustration 16: Shrinkage of prisms; 2nd ES.

3.4 Load tests on prisms prisms (4 x 4 x 16 cm) after 1, 3, 7, 14 and 28 days

The prisms manufactured while the sample areas were being laid were used to measure the shrinkage as well as the compressive strength and the flexural tensile strength. The structural strength of the three prisms was tested on the aforementioned days.

| | Compressive str | ength [N/mm ²] | Flexural tensile strength [N/mm ²] | | |
|------|-----------------------|----------------------------|--|------------|--|
| Days | Comparison mixture | RenoScreed | Comparison mixture | RenoScreed | |
| 1 | 10.6 | 20.9 | 2.2 | 4.2 | |
| 3 | 21.0 | 44.3 | 4.0 | 6.8 | |
| 7 | 29.9 | 52.3 | 5.2 | 7.1 | |
| 14 | 35.5 | 64.4 | 5.5 | 8.2 | |
| 28 | 39.2 | 71.5 | 6.5 | 9.1 | |

Table 8: Compressive strength and flexural tensile strength values; 1st ES.



Illustration 17: Compressive strength of both mixtures; 1st ES.



Illustration 18: Flexural tensile strength of both mixtures; 1st ES.

| | Compressive str | rength [N/mm ²] | Flexural tensile strength [N/mm ²] | | |
|------|-----------------------|-----------------------------|--|------------|--|
| Days | Comparison mixture | RenoScreed | Comparison mixture | RenoScreed | |
| 1 | 5.9 | 17.8 | 1.2 | 3.4 | |
| 3 | 14.1 | 36.3 | 2.9 | 6.1 | |
| 7 | 18.1 | 43.1 | 2.3 | 6.2 | |
| 14 | 24.0 | 49.4 | 3.9 | 6.6 | |
| 28 | 31.0 | 63.0 | 5.1 | 8.5 | |

Table 9: Compressive strength and flexural tensile strength values; 2nd ES.



Illustration 19: Compressive strength values; 2nd ES (both mixtures).



Illustration 20: Flexural tensile strength values; 2nd ES (both mixtures).

3.5 Load tests on plate samples and results of the confirmation test

For the confirmation test of the first experimental series, plates of each sample area were cut out dry. To measure the compressive strength, strips were cut out of the sample areas with a length : width relation of 1 : 1.

To measure the flexural tensile strength, the extracted plates were cut into test pieces with a width of 6 cm and then cut to the corresponding length, their thickness being about 6 times the width. Afterwards these specimens were tested by using the 3-point bending test for determining the flexural tensile strength, the thickness being 5 times the span.

The following tables and graphs show the compressive strength and the flexural tensile strength values measured and tested with the comparison mixture.

| Sample | Width 1 | h 1 Width 2 | | Breaking | Compre | essive strength |
|-----------|---------|-------------|---------|-------------|----------------------|----------------------|
| no. | widui i | widui 2 | neigiii | load | | Average |
| | [mm] | [mm] | [mm] | [N] | [N/mm ²] | [N/mm ²] |
| | | | Cor | nparison mi | ixture | |
| Null LV 1 | 33.4 | 32.7 | 33.3 | 22.205 | 20.34 | |
| Null LV 2 | 33.5 | 34.5 | 33.8 | 21.312 | 18.45 | |
| Null LV 3 | 33.0 | 33.5 | 33.3 | 19.586 | 17.73 | |
| Null LV 4 | 33.4 | 32.5 | 32.9 | 22.203 | 20.42 | 19.53 |
| Null LV 5 | 34.9 | 33.8 | 32.5 | 29.296 | 24.87 | |
| Null LV 6 | 34.7 | 33.9 | 32.6 | 14.123 | 12.02 | |
| Null LV 7 | 33.8 | 34.7 | 32.4 | 26.779 | 22.88 | |
| Null LH 1 | 30.4 | 31.2 | 30.2 | 16.507 | 17.36 | |
| Null LH 2 | 30.7 | 31.6 | 30.7 | 16.261 | 16.80 | |
| Null LH 3 | 30.6 | 31.5 | 32.1 | 13.867 | 14.35 | 15.21 |
| Null LH 4 | 30.4 | 31.6 | 31.1 | 15.818 | 16.46 | |
| Null LH 5 | 30.8 | 31.6 | 31.4 | 10.743 | 11.05 | |

Table 10: Compressive strength values; 1st ES (comparison mixture).

("Null" = comparison mixture)





| Test | Sample | Span | Test | Test speed | | Site o | f fracture | Flexural tensile strength | |
|----------|----------|------|------------------------|------------|---------|--------|------------|------------------------------|----------------------|
| date | no. | Span | 1000 | speed | load | Width | Thickness | | Average |
| | | [mm] | [N/mm ² *s] | [N/s] | [N] | [mm] | [mm] | [N/mm ²] | [N/mm ²] |
| | | | Co | mparison r | nixture | | | | |
| 09.08.07 | N - LV 1 | 146 | 0.1 | 22.1 | 1.483 | 60.8 | 27.8 | 6.92 | |
| 09.08.07 | N - LV 2 | 146 | 0.1 | 26.2 | 854 | 61.0 | 31.6 | 3.08 | |
| 09.08.07 | N - LV 3 | 146 | 0.1 | 25.6 | 969 | 60.2 | 30.3 | 3.83 | |
| 09.08.07 | N - LV 4 | 146 | 0.1 | 25.0 | 1.201 | 60.2 | 30.0 | 4.85 | 5 71 |
| 09.08.07 | N - LV 5 | 146 | 0.1 | 23.8 | 1.933 | 59.7 | 29.4 | 8.24 | 5.74 |
| 09.08.07 | N - LV 6 | 146 | 0.1 | 24.0 | 1.754 | 60.8 | 28.4 | 7.82 | |
| 09.08.07 | N - LV 7 | 146 | 0.1 | 21.5 | 833 | 60.2 | 27.5 | 3.99 | |
| 09.08.07 | N - LV 8 | 146 | 0.1 | 20.4 | 1.432 | 60.3 | 27.0 | 7.17 | |
| 09.08.07 | N - LH 1 | 155 | 0.1 | 24.8 | 945 | 60.6 | 30.8 | 3.83 | |
| 09.08.07 | N - LH 2 | 155 | 0.1 | 23.9 | 849 | 60.8 | 29.3 | 3.78 | |
| 09.08.07 | N - LH 3 | 155 | 0.1 | 21.7 | 1.497 | 60.1 | 31.3 | 5.90 | |
| 09.08.07 | N - LH 4 | 155 | 0.1 | 25.9 | 1.267 | 59.8 | 32.0 | 4.80 | 5 1 5 |
| 09.08.07 | N - LH 5 | 155 | 0.1 | 24.3 | 701 | 59.8 | 30.4 | 2.94 | 5.15 |
| 09.08.07 | N - LH 6 | 155 | 0.1 | 27.5 | 1.317 | 59.4 | 32.8 | 4.78 | |
| 09.08.07 | N - LH 7 | 155 | 0.1 | 25.9 | 1.762 | 60.7 | 29.0 | 8.05 | |
| 09.08.07 | N - LH 8 | 155 | 0.1 | 24.2 | 1.707 | 60.2 | 30.4 | 7.14 | |

Table 11: Flexural tensile strength values; 1st ES (comparison mixture).





Illustration 22: Flexural tensile strength values; 1st ES (comparison mixture).

The compressive strength tests with *RenoScreed* were conducted in accordance with the tests of the comparison mixture. The next table illustrates the compressive strength values.

| Samula | Width 1 | Width 2 | Height | Breaking | Compressive strength | | | | |
|------------|----------|---------|---------|----------|----------------------|----------------------|--|--|--|
| no | widdii i | | Tieigin | load | | Average | | | |
| 110. | [mm] | [mm] | [mm] | [N] | [N/mm ²] | [N/mm ²] | | | |
| RenoScreed | | | | | | | | | |
| Reno RV 1 | 29.7 | 29.8 | 28.2 | 14.622 | 16.53 | | | | |
| Reno RV 2 | 29.6 | 30.0 | 28.0 | 31.821 | 35.88 | | | | |
| Reno RV 3 | 29.3 | 29.2 | 29.5 | 16.600 | 19.41 | 26 77 | | | |
| Reno RV 4 | 29.9 | 29.4 | 27.8 | 32.445 | 36.95 | 20.77 | | | |
| Reno RV 5 | 29.6 | 29.6 | 28.4 | 30.264 | 34.55 | | | | |
| Reno RV 6 | 29.3 | 29.9 | 30.0 | 15.108 | 17.28 | | | | |
| Reno RH 1 | 23.3 | 23.4 | 23.5 | 14.755 | 27.10 | | | | |
| Reno RH 2 | 23.5 | 23.3 | 23.3 | 14.918 | 27.27 | | | | |
| Reno RH 3 | 23.5 | 23.3 | 23.7 | 19.667 | 35.80 | | | | |
| Reno RH 4 | 23.5 | 23.4 | 24.5 | 18.277 | 33.32 | 30.73 | | | |
| Reno RH 5 | 23.6 | 23.0 | 24.4 | 16.927 | 31.24 | 50.75 | | | |
| Reno RH 6 | 23.1 | 23.3 | 23.2 | 15.555 | 29.00 | | | | |
| Reno RH 7 | 23.4 | 23.3 | 23.9 | 16.825 | 30.85 | | | | |
| Reno RH 8 | 23.6 | 23.3 | 24.0 | 17.185 | 31.28 | | | | |

Table 12: Compressive strength values; 1st ES (*RenoScreed*).



Illustration 23: Compressive strength values; 1st ES (*RenoScreed*).

The following table illustrates the results of the *RenoScreed* composition from the confirmation test:

| Test | Sample | Span | Span Test speed | | Breaking | Site c | of fracture | Flexural tensile strength | |
|------------|-----------|------|------------------------|-------|-----------------|--------|-------------|------------------------------|----------------------|
| date | no. | opun | | | ° p••• * | | load | Width | Thickness |
| | | [mm] | [N/mm ² *s] | [N/s] | [N] | [mm] | [mm] | [N/mm ²] | [N/mm ²] |
| RenoScreed | | | | | | | | | |
| 09.08.07 | RS - RV 1 | 136 | 0.1 | 21.9 | 1.816 | 60.6 | 26.6 | 8.64 | |
| 09.08.07 | RS - RV 2 | 136 | 0.1 | 23.6 | 1.636 | 60.9 | 27.7 | 7.13 | |
| 09.08.07 | RS - RV 3 | 136 | 0.1 | 21.0 | 1.703 | 60.6 | 25.9 | 8.53 | |
| 09.08.07 | RS - RV 4 | 136 | 0.1 | 21.0 | 1.759 | 60.8 | 26.3 | 8.50 | 8.09 |
| 09.08.07 | RS - RV 5 | 136 | 0.1 | 21.9 | 1.484 | 60.5 | 26.3 | 7.22 | |
| 09.08.07 | RS - RV 6 | 136 | 0.1 | 22.2 | 1.944 | 60.4 | 27.3 | 8.81 |] |
| 09.08.07 | RS - RV 7 | 136 | 0.1 | 21.4 | 1.680 | 60.4 | 26.9 | 7.82 | |
| 09.08.07 | RS - RH 1 | 132 | 0.1 | 21.7 | 1.886 | 60.4 | 26.1 | 9.04 | |
| 09.08.07 | RS - RH 2 | 132 | 0.1 | 21.5 | 1.615 | 61.0 | 25.9 | 7.84 | |
| 09.08.07 | RS - RH 3 | 132 | 0.1 | 20.1 | 1.469 | 60.6 | 25.6 | 7.33 | ļ |
| 09.08.07 | RS - RH 4 | 132 | 0.1 | 21.3 | 1.638 | 60.2 | 27.0 | 7.39 | 7.67 |
| 09.08.07 | RS - RH 5 | 132 | 0.1 | 20.9 | 1.366 | 61.2 | 27.1 | 6.02 | 1.07 |
| 09.08.07 | RS - RH 6 | 132 | 0.1 | 22.0 | 1.670 | 59.9 | 26.5 | 7.87 | |
| 09.08.07 | RS - RH 7 | 132 | 0.1 | 20.6 | 1.695 | 60.7 | 25.3 | 8.66 | |
| 09.08.07 | RS - RH 8 | 132 | 0.1 | 21.5 | 1.554 | 60.8 | 26.5 | 7.24 | |

Table 13: Flexural tensile strength values; 1st ES (*RenoScreed*).



Illustration 24: Flexural tensile strength values; 1st ES (*RenoScreed*).

For the second experimental series the same test programme was conducted as in the first experimental series. Since the four slabs show different thicknesses, twice the number of slabs, strips and cubes were needed for the test.

The following table gives an overview of the compressive strength values of the comparison mixture from the second experimental series:

| Test | | Width 1 | Width 2 | Hoight | Breaking | Compressive strength | | | | |
|---|----------|---------|-------------|-------------|----------|----------------------|----------------------|--|--|--|
| date | no. | widthi | width 2 | neight | load | | Average | | | |
| | | [mm] | [mm] | [mm] | [N] | [N/mm ²] | [N/mm ²] | | | |
| Comparison mixture $65 + 20 \text{ mm}$ | | | | | | | | | | |
| 22.10.07 | N 65 1.1 | 63.3 | 63.4 | 62.4 | 60.258 | 15.0 | | | | |
| 22.10.07 | N 65 1.2 | 63.2 | 62.8 | 64.1 | 69.667 | 17.6 | | | | |
| 22.10.07 | N 65 1.3 | 63.3 | 64.0 | 63.8 | 71.170 | 17.6 | 17.0 | | | |
| 22.10.07 | N 65 1.4 | 62.8 | 63.4 | 63.7 | 71.689 | 18.0 | | | | |
| 22.10.07 | N 65 1.5 | 62.7 | 63.7 | 63.0 | 68.112 | 17.1 | | | | |
| 22.10.07 | N 65 2.1 | 66.3 | 66.1 | 66.5 | 77.412 | 17.7 | | | | |
| 22.10.07 | N 65 2.2 | 65.8 | 66.6 | 66.5 | 79.646 | 18.2 | | | | |
| 22.10.07 | N 65 2.3 | 66.3 | 67.2 | 66.8 | 74.566 | 16.7 | 16.2 | | | |
| 22.10.07 | N 65 2.4 | 66.5 | 66.4 | 64.5 | 70.183 | 15.9 | | | | |
| 22.10.07 | N 65 2.5 | 58.4 | 59.4 | 59.6 | 42.797 | 12.3 | | | | |
| | | Con | nparison mi | ixture 45 + | 20 mm | | | | | |
| 22.10.07 | N 45 1.1 | 46.9 | 46.4 | 47.2 | 27.204 | 12.5 | | | | |
| 22.10.07 | N 45 1.2 | 46.4 | 46.5 | 47.5 | 33.674 | 15.6 | | | | |
| 22.10.07 | N 45 1.3 | 46.5 | 46.5 | 45.7 | 31.058 | 14.4 | 14.5 | | | |
| 22.10.07 | N 45 1.4 | 46.2 | 46.0 | 44.9 | 32.064 | 15.1 | | | | |
| 22.10.07 | N 45 1.5 | 46.3 | 47.0 | 46.4 | 32.030 | 14.7 | | | | |
| 22.10.07 | N 45 2.1 | 47.6 | 47.4 | 46.4 | 34.706 | 15.4 | | | | |
| 22.10.07 | N 45 2.2 | 47.5 | 47.4 | 47.3 | 23.128 | 10.3 | | | | |
| 22.10.07 | N 45 2.3 | 46.5 | 47.7 | 47.5 | 29.028 | 13.1 | 13.4 | | | |
| 22.10.07 | N 45 2.4 | 45.3 | 45.7 | 43.7 | 32.432 | 15.7 | | | | |
| 22.10.07 | N 45 2.5 | 47.2 | 47.5 | 46.5 | 28.273 | 12.6 | | | | |

Table 14: Compressive strength values; 2nd ES (comparison mixture).

The results from the table above are shown in the following illustrations:



Illustration 25: Compressive strength values – comparison mixture (65 + 20 mm); 2^{nd} ES.



Illustration 26: Compressive strength values – comparison mixture (45 + 20 mm); 2^{nd} ES.

The next table lists the flexural tensile strength values of the comparison mixture from the second experimental series:

| Test Sample | | Span | Test speed | | Breaking | Site of | fracture | Flexural tensile strength | | |
|-------------------------------|-------------------------------|------|------------------------|-------|----------|---------|-----------|------------------------------|----------------------|--|
| date | no. | | | | IOad | Width | Thickness | | Average | |
| | | [mm] | [N/mm ² *s] | [N/s] | [N] | [mm] | [mm] | [N/mm ²] | [N/mm ²] | |
| Comparison mixture 65 + 20 mm | | | | | | | | | | |
| 12.08.07 | N 65 1.1 | 318 | 0.1 | 50.0 | 1.947 | 58.7 | 44.0 | 8.2 | | |
| 12.08.07 | N 65 1.2 | 318 | 0.1 | 49.3 | 1.958 | 59.4 | 61.9 | 4.1 |] | |
| 12.08.07 | N 65 1.3 | 318 | 0.1 | 48.0 | 1.478 | 59.5 | 64.2 | 2.9 | 6.4 | |
| 12.08.07 | N 65 1.4 | 318 | 0.1 | 54.2 | 2.245 | 59.8 | 45.5 | 8.6 | • | |
| 12.08.07 | N 65 1.5 | 318 | 0.1 | 50.5 | 2.052 | 59.8 | 44.2 | 8.4 | | |
| 12.08.07 | N 65 2.1 | 322 | 0.1 | 51.4 | 2.078 | 59.1 | 44.2 | 8.7 | | |
| 12.08.07 | N 65 2.2 | 322 | 0.1 | 48.4 | 1.600 | 59.1 | 39.5 | 8.4 | 1 | |
| 12.08.07 | N 65 2.3 | 322 | 0.1 | 55.0 | 2.197 | 60.7 | 38.3 | 11.9 | 8.3 | |
| 12.08.07 | N 65 2.4 | 322 | 0.1 | 51.5 | 1.401 | 59.3 | 47.8 | 5.0 | • | |
| 12.08.07 | N 65 2.5 | 322 | 0.1 | 49.4 | 1.556 | 59.7 | 40.8 | 7.6 | | |
| | Comparison mixture 45 + 20 mm | | | | | | | | | |
| 12.08.07 | N 45 1.1 | 228 | 0.1 | 33.5 | 1.910 | 60.5 | 43.0 | 5.8 | | |
| 12.08.07 | N 45 1.2 | 228 | 0.1 | 39.6 | 2.238 | 59.9 | 47.1 | 5.8 | 1 | |
| 12.08.07 | N 45 1.3 | 228 | 0.1 | 39.2 | 1.814 | 59.7 | 46.3 | 4.8 | 5.6 | |
| 12.08.07 | N 45 1.4 | 228 | 0.1 | 38.1 | 1.995 | 59.7 | 46.5 | 5.3 | | |
| 12.08.07 | N 45 1.5 | 228 | 0.1 | 31.8 | 2.016 | 59.9 | 42.9 | 6.2 |] | |
| 12.08.07 | N 45 2.1 | 240 | 0.1 | 38.2 | 1.518 | 59.8 | 48.2 | 3.9 | | |
| 12.08.07 | N 45 2.2 | 240 | 0.1 | 39.6 | 1.012 | 60.2 | 45.7 | 2.9 | | |
| 12.08.07 | N 45 2.3 | 240 | 0.1 | 38.5 | 1.181 | 60.3 | 45.7 | 3.4 | 3.2 | |
| 12.08.07 | N 45 2.4 | 240 | 0.1 | 39.3 | 1.424 | 60.0 | 47.5 | 3.8 | | |
| 12.08.07 | N 45 2.5 | 240 | 0.1 | 36.4 | 576 | 59.9 | 43.8 | 1.8 | | |

Table 15: Flexural tensile strength values; 2nd ES (comparison mixture).



Illustration 27: Flexural tensile strength of the comparison mixture (65 + 20 mm); 2^{nd} ES.





The compressive strength values of *RenoScreed* were determined in the same way as the comparison mixture. The next table lists the compressive strength values of *RenoScreed*, 2^{nd} ES.

| Test Sample | | Width 1 Width 2 | | Height | Breaking | Compressive strength | | |
|-------------|----------|-----------------|----------|----------------------|----------|----------------------|----------------------|--|
| date | no. | With I | Widdii 2 | mengint | load | | Average | |
| | | [mm] | [mm] | [mm] | [N] | [N/mm ²] | [N/mm ²] | |
| | | | | | | | | |
| 22.10.07 | R 55 1.1 | 51,0 | 50,6 | 52,0 | 78.102 | 30,3 | | |
| 22.10.07 | R 55 1.2 | 50,8 | 51,0 | 51,3 | 82.474 | 31,8 | | |
| 22.10.07 | R 55 1.3 | 51,0 | 51,5 | 51,1 | 77.983 | 29,7 | 30,8 | |
| 22.10.07 | R 55 1.4 | 50,9 | 51,2 | 51,1 | 77.051 | 29,6 | | |
| 22.10.07 | R 55 1.5 | 50,7 | 51,1 | 51,1 | 84.292 | 32,5 | | |
| 22.10.07 | R 55 2.1 | 53,8 | 53,9 | 53,4 | 69.150 | 23,8 | | |
| 22.10.07 | R 55 2.2 | 51,4 | 53,9 | 54,3 | 60.905 | 22,0 | | |
| 22.10.07 | R 55 2.3 | 53,4 | 52,9 | 52,8 | 85.209 | 30,2 | 26,8 | |
| 22.10.07 | R 55 2.4 | 53,5 | 53,6 | 53,7 | 86.846 | 30,3 | | |
| 22.10.07 | R 55 2.5 | 52,7 | 53,8 | 52,8 | 78.104 | 27,5 | | |
| | | | RenoScr | <i>reed</i> $35 + 2$ | 20 mm | | | |
| 22.10.07 | R 35 1.1 | 38,6 | 38,6 | 37,1 | 39.582 | 26,6 | | |
| 22.10.07 | R 35 1.2 | 38,8 | 38,7 | 35,8 | 43.494 | 29,0 | | |
| 22.10.07 | R 35 1.3 | 38,4 | 38,3 | 38,1 | 38.481 | 26,2 | 29,2 | |
| 22.10.07 | R 35 1.4 | 38,4 | 38,5 | 37,4 | 50.827 | 34,4 | | |
| 22.10.07 | R 35 1.5 | 38,4 | 37,8 | 37,4 | 43.576 | 30,0 | | |
| 22.10.07 | R 35 2.1 | 34,6 | 34,2 | 34,3 | 31.842 | 26,9 | | |
| 22.10.07 | R 35 2.2 | 34,8 | 34,6 | 34,4 | 37.694 | 31,3 | | |
| 22.10.07 | R 35 2.3 | 34,7 | 34,7 | 34,2 | 32.471 | 27,0 | 28,6 | |
| 22.10.07 | R 35 2.4 | 34,8 | 34,8 | 33,9 | 39.476 | 32,6 | | |
| 22.10.07 | R 35 2.5 | 34,8 | 34,6 | 34,6 | 30.230 | 25,1 | | |

Table 16: Compressive strength values of the screed slabs; 2nd ES (*RenoScreed*).



Illustration 29: Compressive strength values of *RenoScreed* (55 + 20 mm); 2nd ES.



Illustration 30: Compressive strength values of *RenoScreed* (35 + 20 mm); 2^{nd} ES.

The flexural tensile strength values of the *RenoScreed* mixture from the 2^{nd} experimental run are listed in the table below:

| Test | Sample | Span | Test speed | | Breaking | Site o | f fracture | Flexura stre | l tensile ngth | |
|-----------------------|---------------------------------|------|------------------------|-------|----------|--------|------------|----------------------|----------------------|--|
| date | no. | 1 | 1 | - | | Width | Thickness | | Average | |
| | | [mm] | [N/mm ² *s] | [N/s] | [N] | [mm] | [mm] | [N/mm ²] | [N/mm ²] | |
| RenoScreed 55 + 20 mm | | | | | | | | | | |
| 23.10.07 | R 55 1.1 | 260 | 0.1 | 42.2 | 1.431 | 58.7 | 30.6 | 10.1 | | |
| 23.10.07 | R 55 1.2 | 260 | 0.1 | 39.9 | 1.476 | 59.2 | 31.1 | 10.0 | - | |
| 23.10.07 | R 55 1.3 | 260 | 0.1 | 40.4 | 1.769 | 58.1 | 30.3 | 12.9 | 12.6 | |
| 23.10.07 | R 55 1.4 | 260 | 0.1 | 42.2 | 1.631 | 59.6 | 29.0 | 12.7 | | |
| 23.10.07 | R 55 1.5 | 260 | 0.1 | 38.7 | 2.508 | 57.8 | 31.1 | 17.5 | | |
| 23.10.07 | R 55 2.1 | 264 | 0.1 | 43.7 | 1.859 | 59.7 | 25.7 | 18.7 | | |
| 23.10.07 | R 55 2.2 | 264 | 0.1 | 41.1 | 1.249 | 60.3 | 25.9 | 12.2 | | |
| 23.10.07 | R 55 2.3 | 264 | 0.1 | 42.6 | 3.922 | 60.0 | 52.7 | 9.3 | 15.2 | |
| 23.10.07 | R 55 2.4 | 264 | 0.1 | 40.5 | 3.380 | 60.5 | 29.6 | 25.2 | | |
| 23.10.07 | R 55 2.5 | 264 | 0.1 | 44.0 | 4.397 | 59.9 | 53.0 | 10.3 | | |
| | RenoScreed $35 + 20 \text{ mm}$ | | | | | | | | | |
| 22.10.07 | R 35 1.1 | 171 | 0.1 | 31.5 | 2.144 | 59.4 | 36.4 | 7.0 | | |
| 22.10.07 | R 35 1.2 | 171 | 0.1 | 28.3 | 1.508 | 60.0 | 30.6 | 6.9 | | |
| 22.10.07 | R 35 1.3 | 171 | 0.1 | 22.4 | 1.488 | 60.5 | 30.3 | 6.9 | 6.2 | |
| 22.10.07 | R 35 1.4 | 171 | 0.1 | 32.2 | 1.459 | 60.0 | 36.7 | 4.6 | | |
| 22.10.07 | R 35 1.5 | 171 | 0.1 | 23.5 | 1.232 | 60.0 | 31.1 | 5.5 | | |
| 23.10.07 | R 35 2.1 | 176 | 0.1 | 26.9 | 1.754 | 59.8 | 34.0 | 6.7 | | |
| 23.10.07 | R 35 2.2 | 176 | 0.1 | 25.2 | 1.286 | 59.8 | 33.5 | 5.0 | | |
| 23.10.07 | R 35 2.3 | 176 | 0.1 | 28.3 | 1.583 | 59.9 | 34.9 | 5.7 | 5.9 | |
| 23.10.07 | R 35 2.4 | 176 | 0.1 | 30.7 | 1.643 | 59.4 | 36.9 | 5.4 | | |
| 23.10.07 | R 35 2.5 | 176 | 0.1 | 29.0 | 1.832 | 59.9 | 35.1 | 6.5 | | |

Table 17: Flexural tensile strength values; 2nd ES (*RenoScreed*).









| | Density [kg/dm ³] (1st ES <u>and</u> 2nd ES) |
|--------------------|---|
| Comparison mixture | 2.01 2.05 |
| RenoScreed | 2.09 2.22 |

3.7. Surface quality (surface tensile strength values, scratch tests, absorbing capacity)

For the determination of the *surface tensile strength* three steel dollies were glued to the surface of each sample area after the edge curling measurement.

The test results are listed in the table below.

| Test series | Area | Mixture | Thick- ness | Test dolly 1 [N/mm ²] | Test dolly 2 [N/mm ²] | Test dolly 3 [N/mm ²] | Average [N/mm ²] |
|----------------|------|-------------|----------------|--------------------------------------|--------------------------------------|--------------------------------------|---------------------------------|
| 1 | 1 | RenoScreed | 35 | 2.07 | 1.95 | 1.17 | 1.73 |
| 1 | 2 | Comp. mixt. | 35 | 0.31 | 0.33 | 0.67 | 0.44 |
| 2 | 1 | RenoScreed | 55 | 1.85 | 2.15 | 0.81 | 1.61 |
| 2 | 2 | RenoScreed | 35 | 2.34 | 1.08 | 1.91 | 1.78 |
| 2 | 3 | Comp. mixt. | 65 | 0.15 | 0.35 | 0.31 | 0.27 |
| 2 | 4 | Comp. mixt. | 45 | 0.19 | 0.13 | 0.05 | 0.13 |

 Table 26: Surface tensile strength values of all sample areas – all fractures within screed structure (see photos below)



RenoScreed

Comparison mixture

In addition, <u>scratch tests</u> were carried out on the surfaces. The results are shown in the photos below.



RenoScreed

Comparison mixture

After the scoring it is assessed how deep the scratches are and whether the edges are broken out at the intersections. Normally, the orthogonal scratch pattern does not lead to deep scratches in conventional cementitious screeds. The scratches can be seen but they are usually hardly palpable. As a rule, the diagonal scratch pattern leaves broken out edges which often leads to misinterpretations. Since there are no valid standards a lot of experience is necessary to judge the result of scratch tests in the correct way.

Sample areas produced with *RenoScreed* showed remarkably good results without "*sintered layers*" on the surface, whereas the comparison mixture showed fairly poor and partially insufficient results.

The surface of the screeds installed with the comparison mixture showed an evidently higher water <u>absorbing capacity</u> than those installed with *RenoScreed* mortar. Still, the absorbing capacity of *RenoScreed* is sufficient for the application of aqueous primers and adhesives.

3.8. Drying period of the sample areas

According to valid standards a screed can be covered as soon as the residual moisture value falls below 2.0 CM-%. The measurement is carried out in compliance with procedure instruction "FBH-AD" from February 2005 [5.8.]. The value is to be determined ten minutes after shutting the CM-tester. The results are influenced by factors such as relative humidity above the screed before the test, position of the sample piece within the screed (drier values at the edges), share of pebbles in the sample piece etc.

The measurements showed the following drying times for the mixtures in question:

- Standard mixture: more than 56 days
- RenoScreed: **7 days**

3.9. Assessment of the additional screed strips with an unfavourable length- width- ratio

Screed strips with unfavourable length-width-ratios are prone to crack development if the screed strength is high. In order to test the tendency toward crack development of the screed mixtures used, a screed strip of 0.3×2.0 m (produced from the *RenoScreed* mixture) was placed into a shutter specially manufactured for this purpose. During the entire test period no cracks were found in this screed strip.

The conclusion to be drawn from this is that at an early stage the mortar applied does not show any detrimental tensions. That is to say the screed strength develops much faster than the inherent tensions caused by the drying and the contraction of the mortar. As a result any unfavourable crack developments are avoided.

3.10. Flatness tolerances on the sample areas according to DIN 18202

The flatness of the sample areas was examined with the help of a measuring rod of 2.0 m length. All sample areas met the requirements according to DIN 18202, table 3, line 4 (i.e. floors with finished surfaces, elevated demands). All flatness variations measured with the above mentioned measuring rod were below 5.0 mm. The distance between the two points of measurement amounted to 2,0 m.

Within a testing period of 52 days the edge curling on the sample areas amounted to a maximum of 2.0 to 3.0 mm in relation to the original surface heights. Edge curling, however, is not subject of DIN 18202.

3.11. Granulometric composition of the mineral aggregate

When the mineral aggregate was delivered, a sample was taken to determine the granulometric composition. The following graphs show the grain size distribution curve of the mineral aggregate.







Illustration 46: Grain size distribution curve of the mineral aggregate; 2nd ES.; A8, B8, C8: grain size distribution curves according to DIN 1045 [5.1.].

In both series the mineral aggregate met the requirements of the grain size distribution "Type B" according to DIN 1045 [5.1.].

3.12. Trafficability

A screed is supposed to be trafficable after reaching a compressive strength value of at least 15 N/mm² [5.6.]. *RenoScreed* reached this value after 24 hrs., the comparison mixture after 3 days.

4. General evaluation and summary

The tests demonstrate that screeds produced with the *RenoScreed* mixture generally hardened significantly faster and showed less shrinkage than the comparison mixture. With *RenoScreed* the usual edge curling deformation set in at a considerably earlier date than with the comparison mixture, which was produced simultaneously using a common screed mortar composition.

Due to their mortar composition and their more opportune water-cement ratios, the screeds produced with *RenoScreed* showed much higher strength values and the final strength was reached earlier.

After three days, screeds produced with the *RenoScreed* mixture showed strength values which a screed manufactured with the comparison mixture first reached after 28 days.

5. References

- 5.1. DIN 1045-2:2001-07 : "Concrete, reinforced and prestressed concrete structures"; Part 2: Concrete - Specification, properties, production and conformity; Application rules for DIN EN 206-1; Amendment A2; att. doc. L
- 5.2. DIN 18202:2005-10 : "Tolerances in building construction; Buildings"
- 5.3. DIN 18560-1:2004-04 : "Floor screeds in building construction"; Part 1: General requirements, testing and construction
- 5.4. DIN 18560-1:2004-04 : "Floor screeds in building construction"; Part 2: Floor screeds and heating floor screeds on insulation layers
- 5.5. DIN EN 13892:2003-02: "Methods of test for screed materials"
- 5.6. DIN 18560, Part 1 and 2: "Floor screeds in building construction"; Mai 1992
- 5.7. BEB-Hinweisblatt: "Oberflächenzug- und Haftzugfestigkeit von Fußböden – Allgemeines, Prüfung, Einflüsse, Beurteilung"; November 2004
- 5.8. BEB-Merkblatt: "Schnittstellenkoordination bei beheizten Fußbodenkonstruktionen Arbeitsanweisung/Dokumentation FBH-AD CM-Messung"; February 2005

6. Photo report

























